

**IRSN**

INSTITUT  
DE RADIOPROTECTION  
ET DE SÛRETÉ NUCLÉAIRE

*Faire avancer la sûreté nucléaire*

# Neutron-gamma flux and dose calculations in a Pressurized Water Reactor (PWR)

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*San Francisco, CA USA*

*ANS SUMMER  
Meeting*

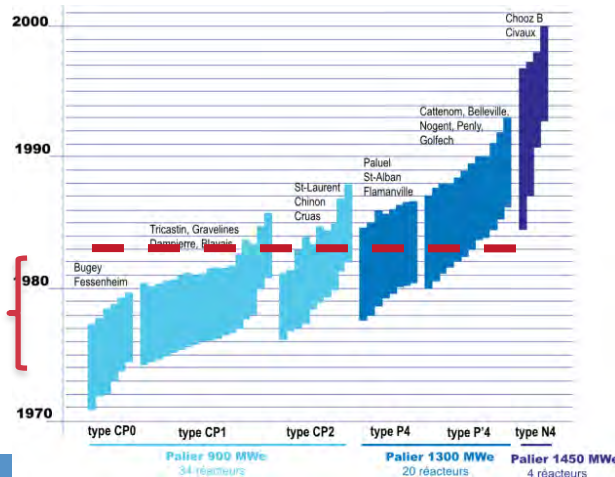
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- Monte Carlo calculations in the PWR
  - ❖ Reactor model - Tihange-1
  - ❖ Fission distribution in the core
  - ❖ Variance reduction parameters
- Results
- Conclusion

## General context

- EDF NPPs initially designed for 40 years
- Feasibility study to extend the duration of NPPs operation
- IRSN: R&D as a support of expertise on safety
  - Mainly concerning non replaceable components: reactor vessel and internals, containment, electrical cables
  - Radiation environment calculation in the nuclear reactor

40 years  
old in 2020



## R&D project

### DISCOMS: Distributed Sensing for Corium Monitoring and Safety

#### Feasibility study of instrumentation implementation:

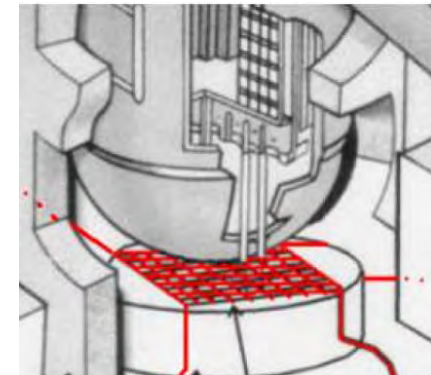
- Optical Fiber Sensors (OFS)
- Self Powered Neutron Detectors (SPNDs)

#### Monitor:

- Status of the third barrier of confinement
- Pressure vessel breakthrough, concrete floor erosion and corium cooling



IRSN in charge of radiation environment calculations: *neutron and gamma dose, flux spectra*



## Monte Carlo simulation of the nuclear reactor

### Monte Carlo codes:

Solve the n- $\gamma$  transport equation using precise geometry & continuous energy cross sections

### Core:

Dimensions ~3.6m x ~3m

Neutron mean free path ~1-2 cm

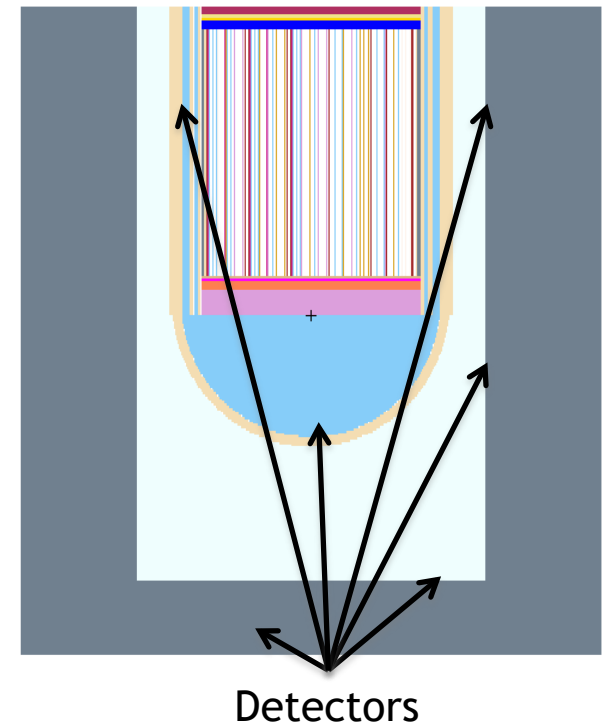
→ To cover the reactor core, a lot of simulated particles are needed

→ Outside the core the flux is strongly attenuated: more simulated particles are needed increasing strongly the calculation time

To rise this challenge

→ Variance reduction techniques are used to increase the statistics for the researched responses

↳ Collaboration with ENEA, Bologna



### Calculation scheme:

Fission distribution  
in the core



Variance reduction  
parameters  
optimisation



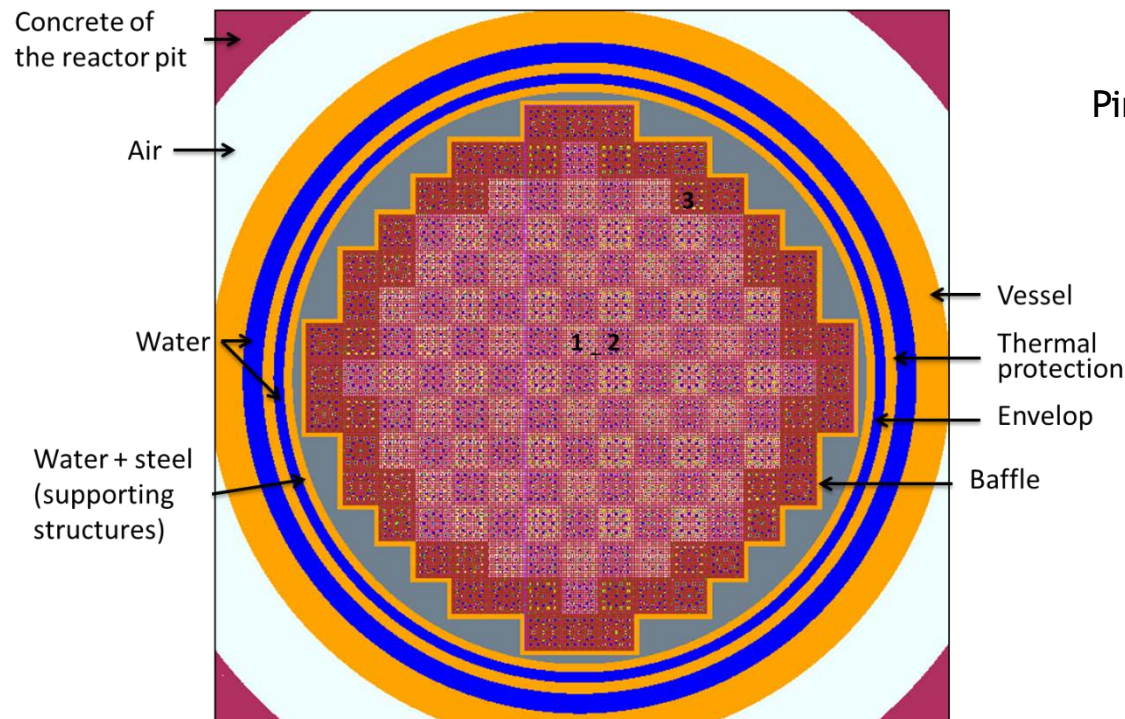
Monte Carlo  
particles transport  
towards detectors

## PWR reactor modelling with MCNP

Core is based on the Tihange-1 reactor in Belgium (public data available, with associated flux in-core distribution measurements, similar to French PWRs)

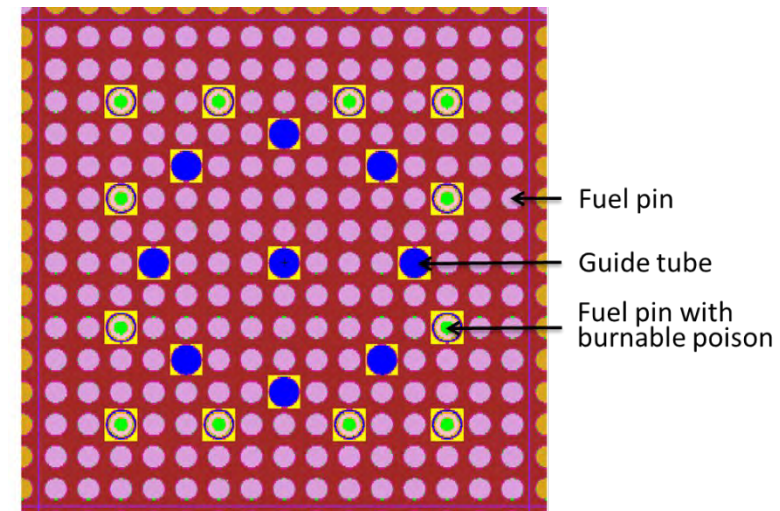
Hot zero power (no thermal gradient)

Fresh fuel (3 types of enrichment with the highest enrichment on the edge of the core)



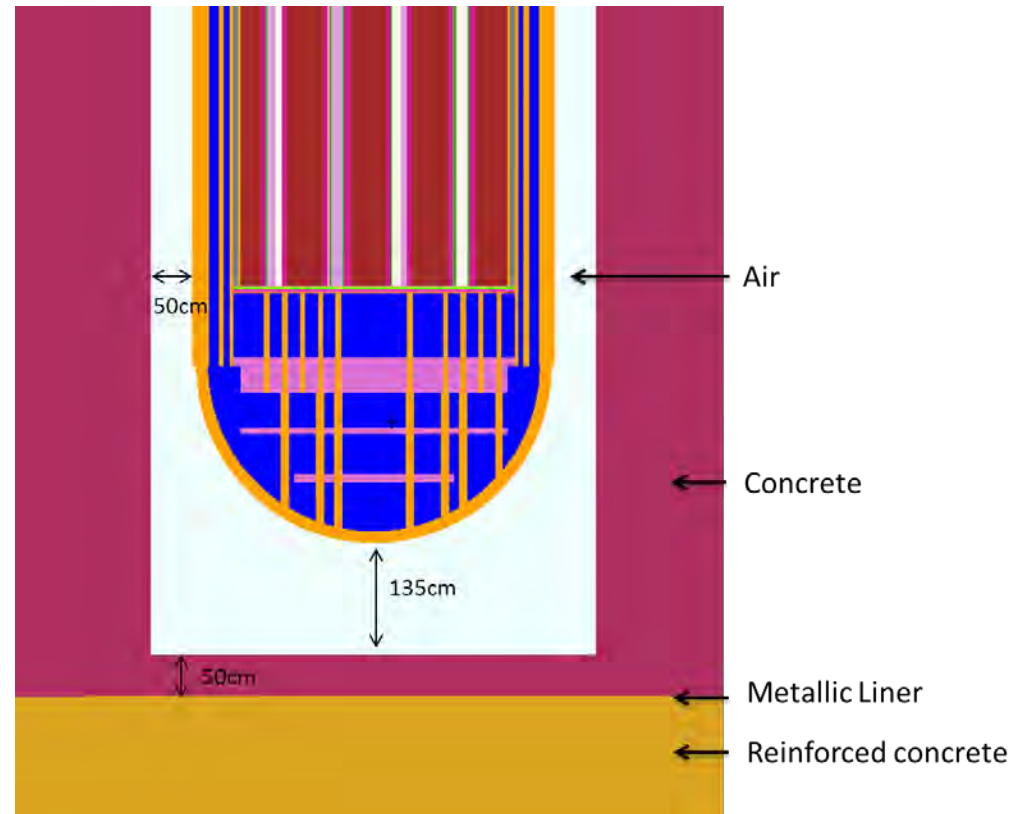
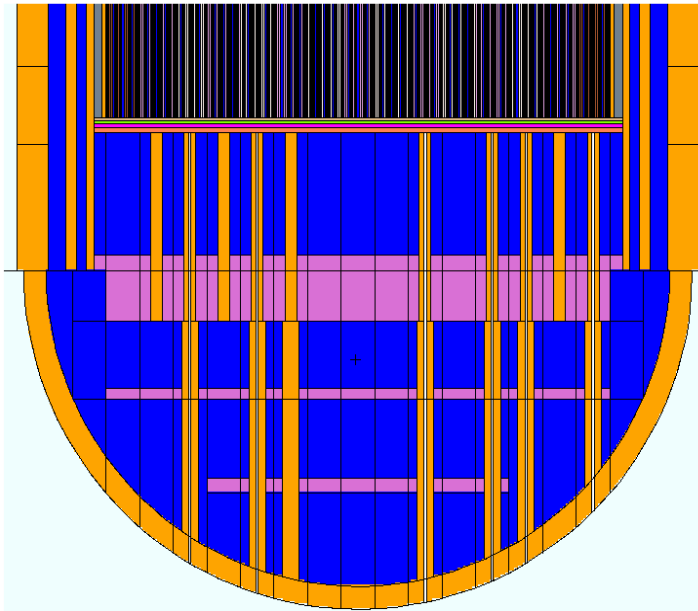
3 types of fuel enrichment  
(1: 2,55 %; 2: 1,95 % and 3: 3,10 %)

### Pin by pin modelling in the MCNP model



## PWR reactor modelling with MCNP

Modelling including structures in the bottom of the vessel and the reactor pit  
(supporting structures, piercing instrumentation tubes ...)

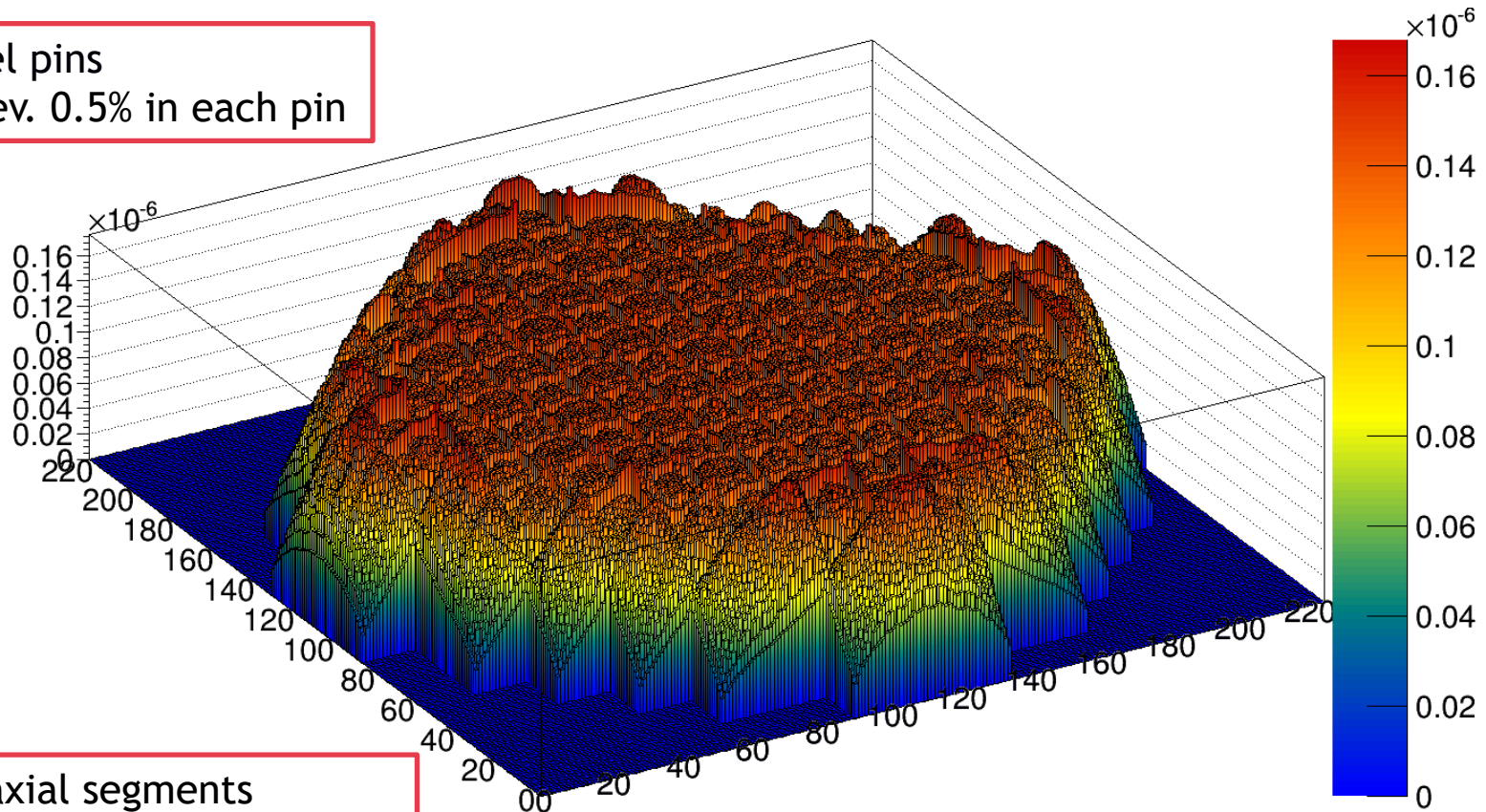


## Calculated fission distribution in the core

### First step:

- Converge the fission distribution in the core (criticality calculation  $\sim 10^{10}$  particles)
- Tally the fission reaction rate in each pin

$\approx 35\ 000$  fuel pins  
max std. dev. 0.5% in each pin



200 axial segments  
(unique distribution for the core)

Used nuclear data base ENDF/B-7.1

## Comparison of calculated fission distribution to experimental data

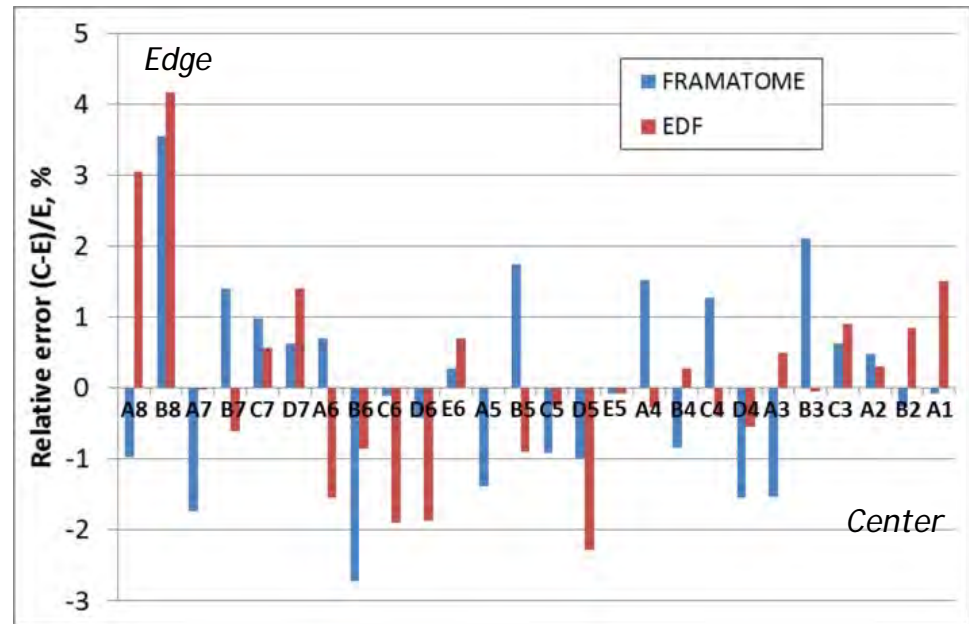
Flux distribution measurements available with two separate measurement campaigns by FRAMATOME and by EDF

→ No measurement uncertainties available

Flux distribution in 1/8<sup>th</sup> of the core:

Comparison of the calculated values:

Center	A	B	C	D	E
1	1.086				
	1.069				
	<b>1.085</b>				
2	1.087	1.081			
	1.089	1.069			
	<b>1.092</b>	<b>1.078</b>			
3	1.090	1.066	1.074		
	1.068	1.089	1.071		
	<b>1.073</b>	<b>1.088</b>	<b>1.081</b>		
4	1.066	1.078	1.076	1.099	
	1.085	1.066	1.094	1.088	
	<b>1.082</b>	<b>1.069</b>	<b>1.090</b>	<b>1.082</b>	
5	1.074	1.050	1.066	1.075	0.901
	1.059	1.078	1.059	1.089	0.901
	<b>1.059</b>	<b>1.068</b>	<b>1.056</b>	<b>1.064</b>	<b>0.900</b>
6	1.049	1.065	0.986	0.940	0.709
	1.073	1.045	1.004	0.954	0.706
	<b>1.056</b>	<b>1.036</b>	<b>0.985</b>	<b>0.936</b>	<b>0.711</b>
7	1.033	1.037	0.968	0.648	
	1.015	1.058	0.972	0.643	
	<b>1.015</b>	<b>1.052</b>	<b>0.977</b>	<b>0.652</b>	
Edge	0.921	0.675			
	0.885	0.671			
	<b>0.912</b>	<b>0.699</b>			



Highest error at the edge of the core (4%)



C-E : same order as discrepancies between both measurements

Used nuclear data base ENDF/B-7.1



## Neutron and gamma responses

### DISCOMS:

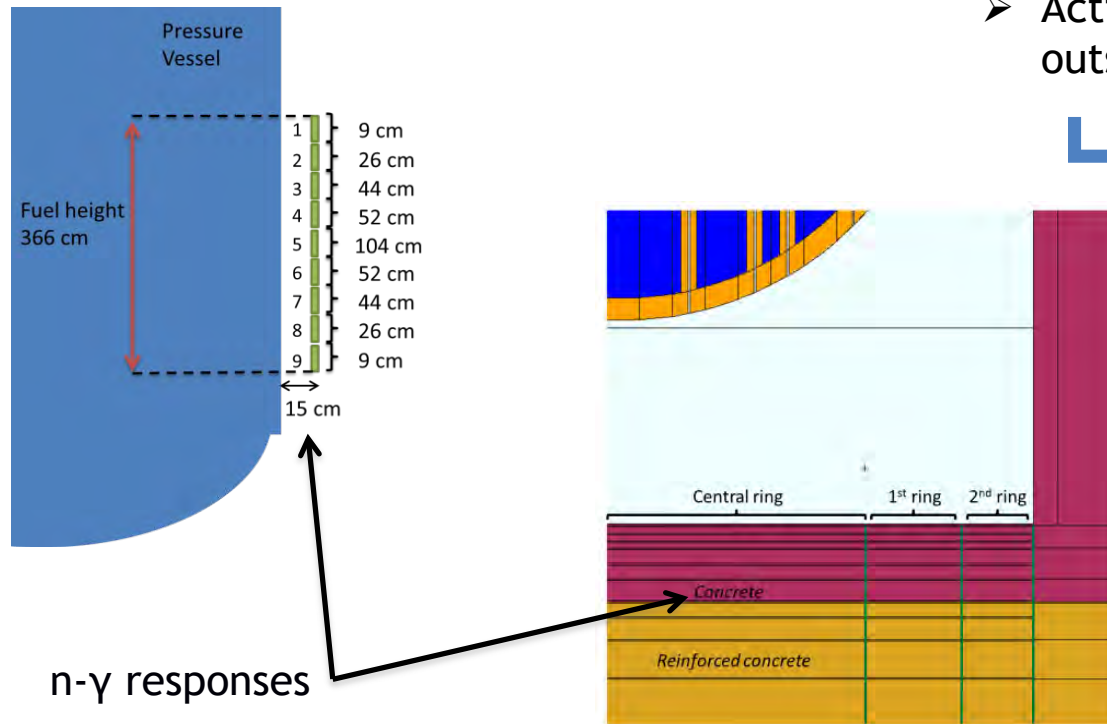
- OFS ➤ fast neutron fluence and gamma dose
- possibility to be embedded in the concrete

- SPNDs ➤ neutron and gamma flux spectra

### Ageing:

- Neutron fluence azimuthal pic on the inner side of the vessel & vessel bottom
- Neutron & gamma fluxes on the concrete
- Activation of internals + structures outside the vessel

↳ **Work still ongoing**

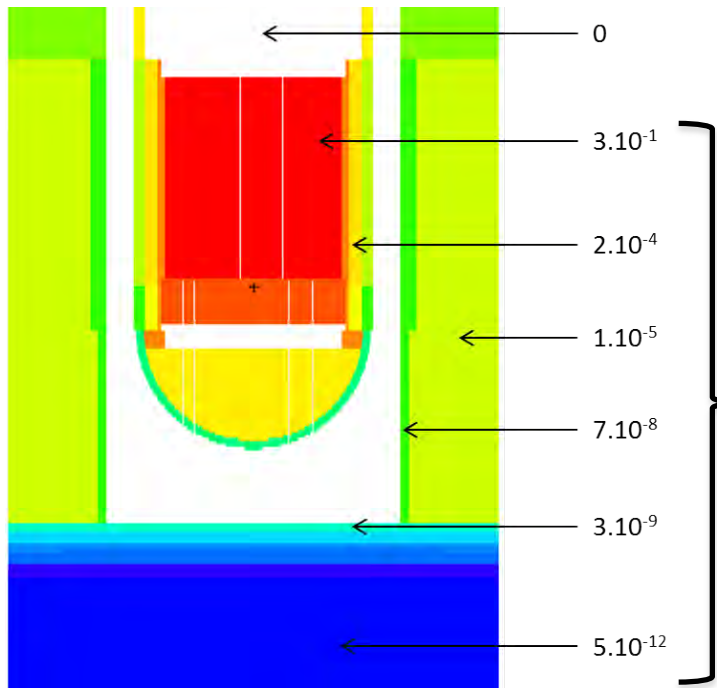


## Variance reduction parameters

### IRSN-ENEA collaboration:

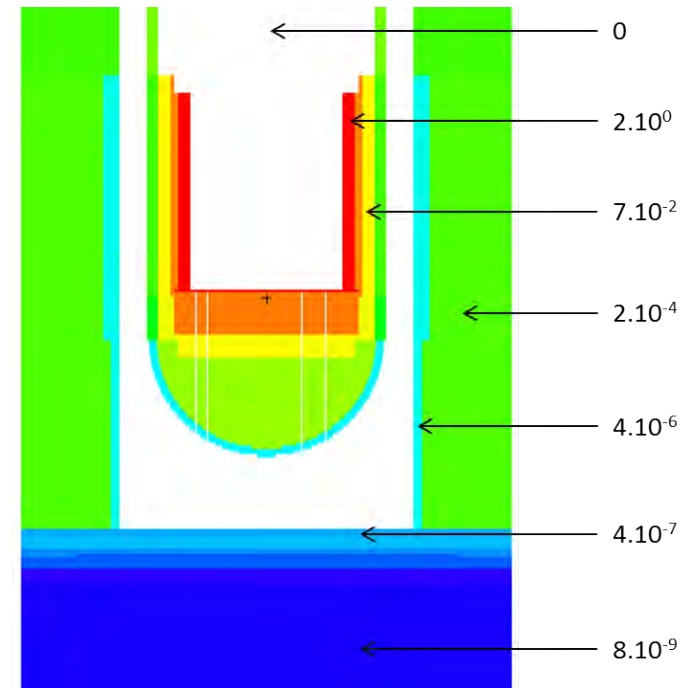
- Kenneth W. Burn (ENEA) calculated the variance reduction parameters using the DSA (Direct Statistical Approach) method optimizing the parameters for the set of the responses of interest: inside and outside the vessel, in the concrete for n and  $\gamma$ .

Weights for neutrons of 2-5 MeV  
(using Weight Windows)

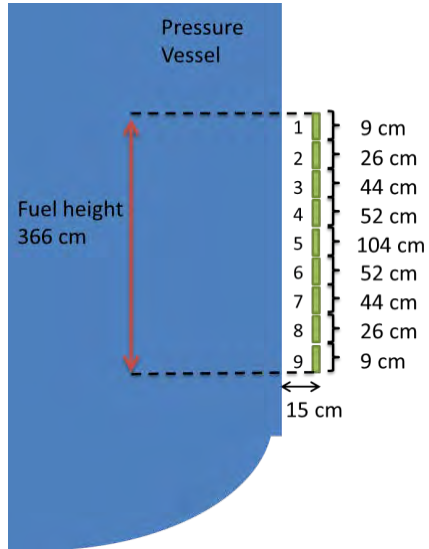


Attenuation  
 $\approx 10^{-12}$

Weights for gamma rays of 0.7-1.5 MeV  
(using Weight Windows)



## Flux on the side of the vessel

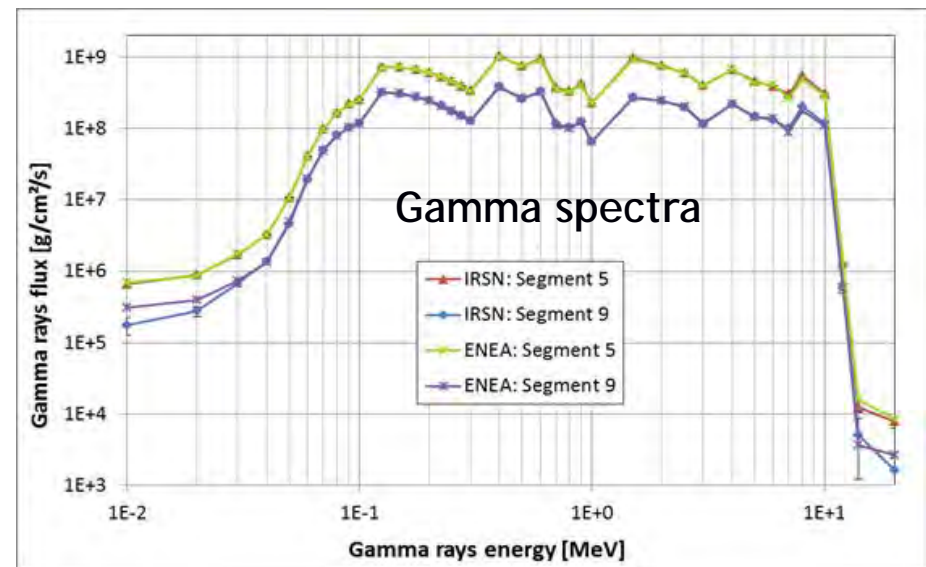
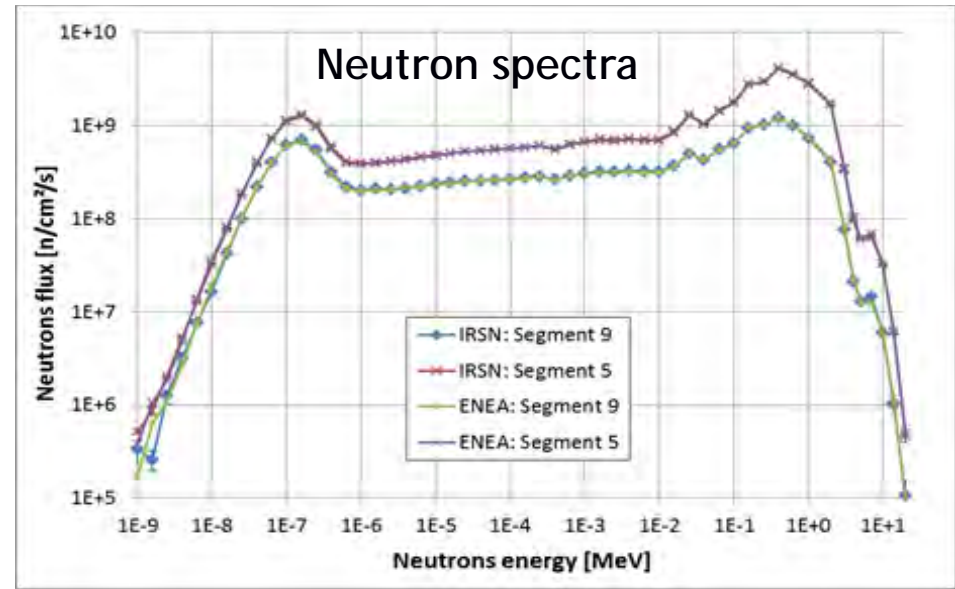


### IRSN & ENEA calculations:

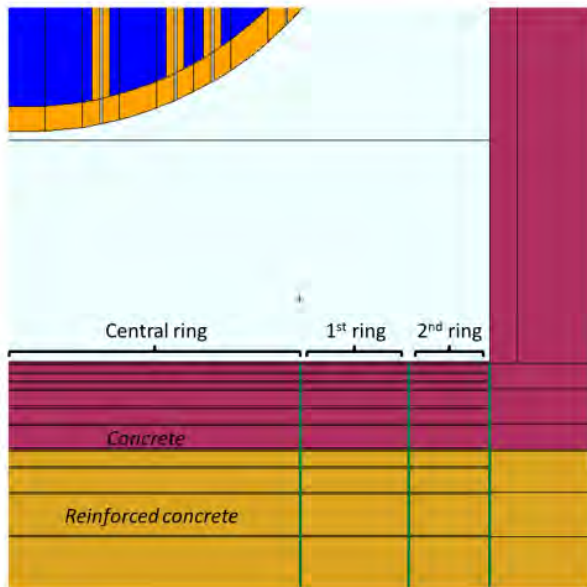
- Use of different source distributions
- Nuclear Data bases
  - IRSN: ENDF/B-VII.1
  - ENEA: JEFF-3.1

➡ Good agreement IRSN/ENEA

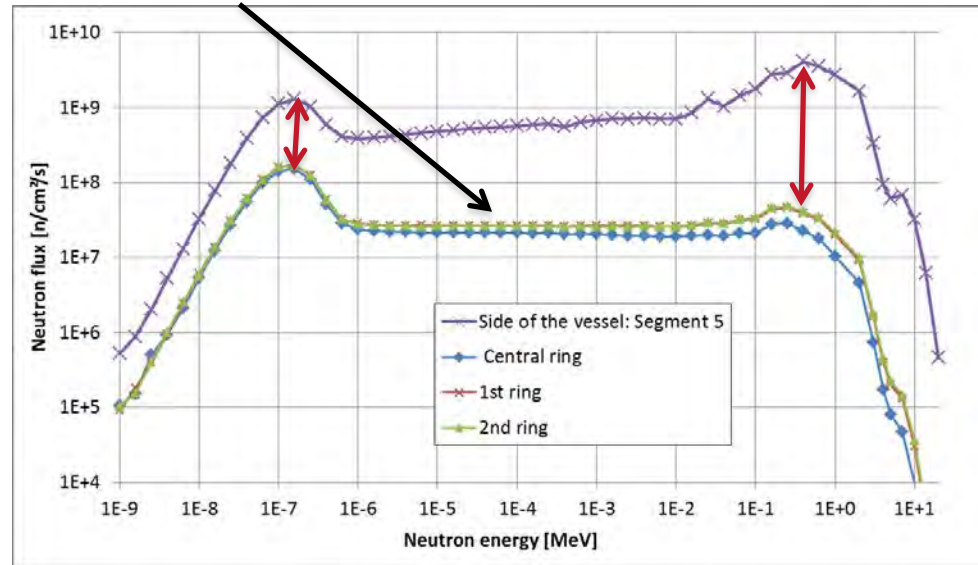
➡ Axial position: no significant impact on n/γ spectra



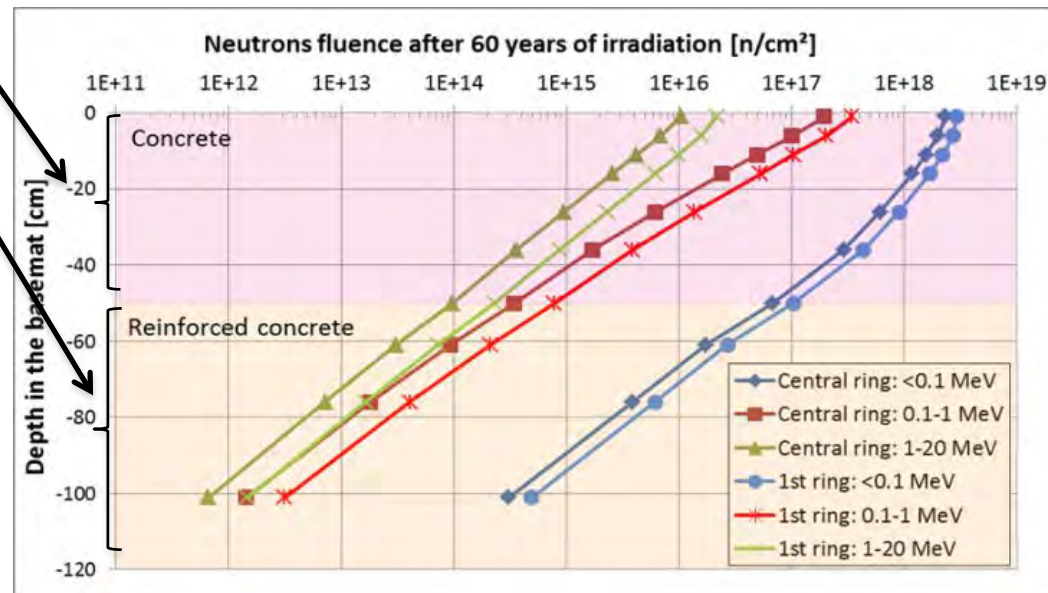
## Neutron flux in the basemat



## Neutron flux on the surface of the basemat



## Neutron fluence attenuation in the concrete



### IRSN calculations:

- ➔ On the basemat surface:
  - Strong impact of the position
  - ✧ Fast neutrons  $\times 10^{-2}$
  - ✧ Thermal neutrons  $\times 10^{-1}$
- ➔ Strong attenuation in the concrete

## Sensitivity study

Example:

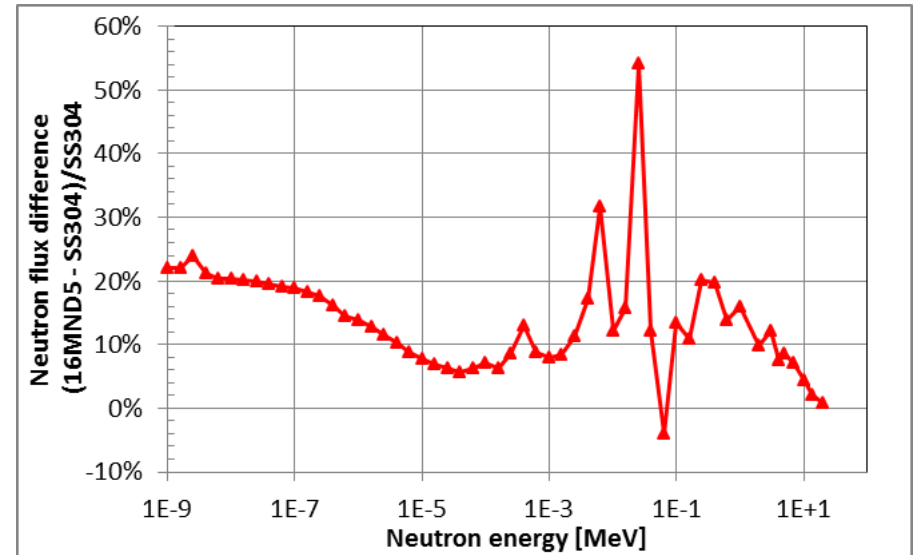
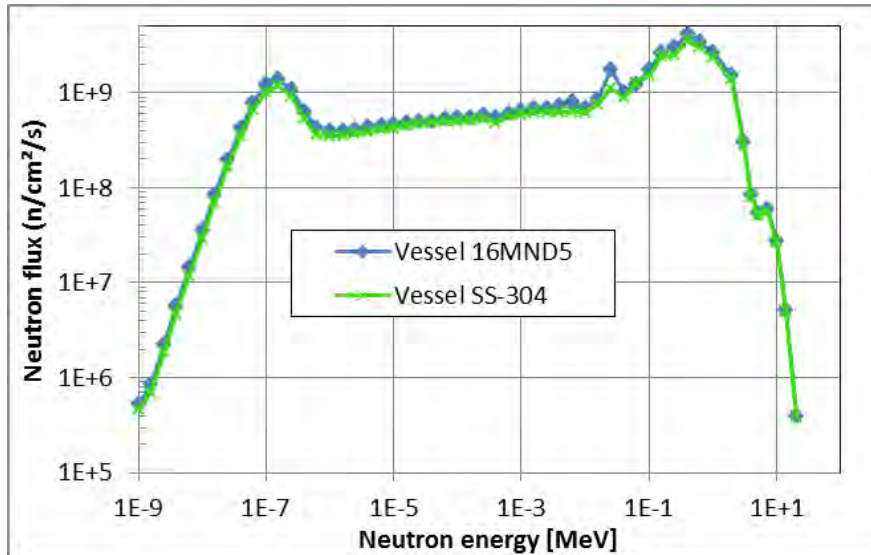
Pressure vessel material replacement

Stainless steel 304 → replaced by 16MND5

Goal: To see the impact of the vessel composition

Main elements	Fe	Cr	Ni	Mn
16MND5	96.8 %	0.3 %	0.7 %	1.4 %
SS-304	66.7 %	20.2 %	11.2 %	2.0 %

### Neutron flux outside the pressure vessel



Flux outside the vessel is sensitive to steel composition

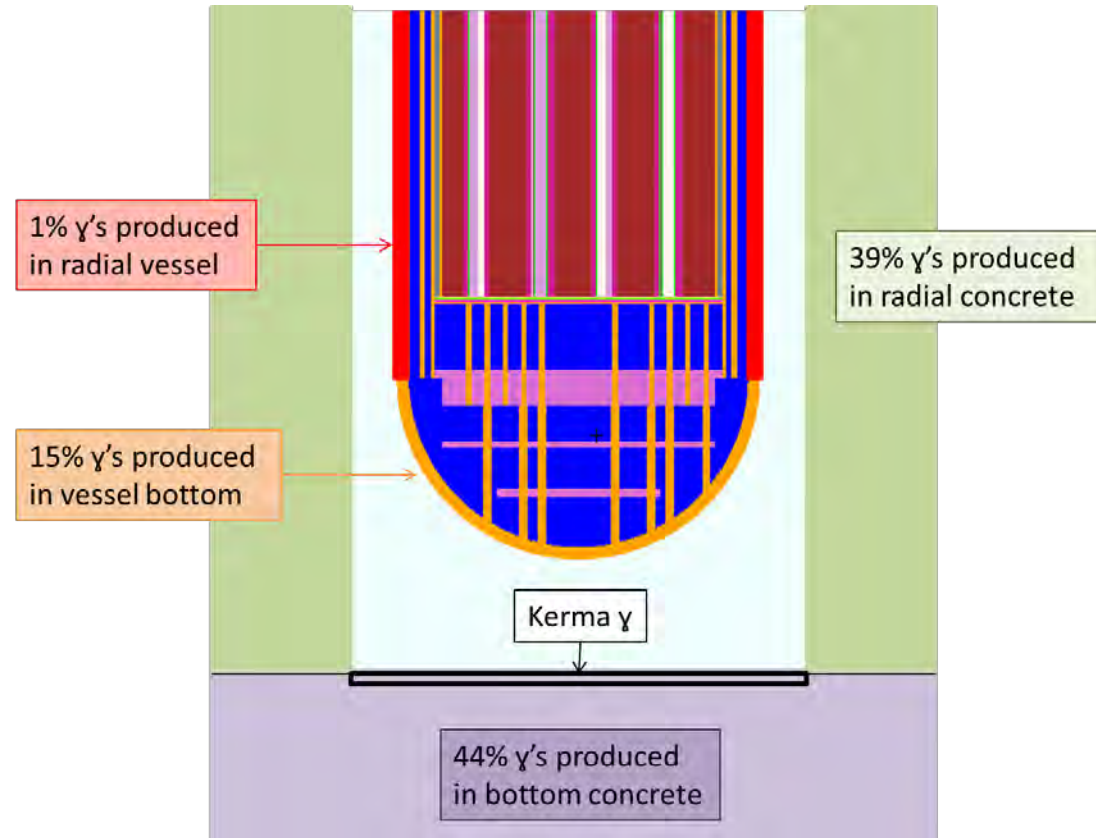
## Gamma production analysis

Example:

Studied response: Kerma  $\gamma$  on the basemat

Flagging of cells where the gammas are produced

Goal: To know which materials are important (need to be known precisely)



Gammas are produced mainly in the concrete and only to 16% in the vessel

## Radiation calculations for ageing issue & R&D project

- Radiation environment can be characterized with “pure” Monte Carlo simulations using variance reduction methods
  - Time consuming calculations, but feasible (burn-up, fission source distribution, variance reduction parameters and final transport calculations)
  - Needs good knowledge of the core and other structures in the reactor
    - ⇒ Analysis/Sensitivity study to search for important parameters (compositions, ...)
- Ageing issue: different physical quantities can be derived from the neutron/gamma flux calculations as Kerma/Dose, DPA, activation, He/H production, ...

*This work was performed thanks to:*

Kenneth Burn (ENEA), Patrizio Camprini (ENEA), Isabelle Duhamel (IRSN), Benjamin Dechenaux (IRSN), Joachim Miss (IRSN), Bernard Chaumont (IRSN), Arthur Peron (IRSN subcontractor), Pietro Signorotti (IRSN subcontractor), Bilel Boussetta (internship), Léa Tillard (internship)

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